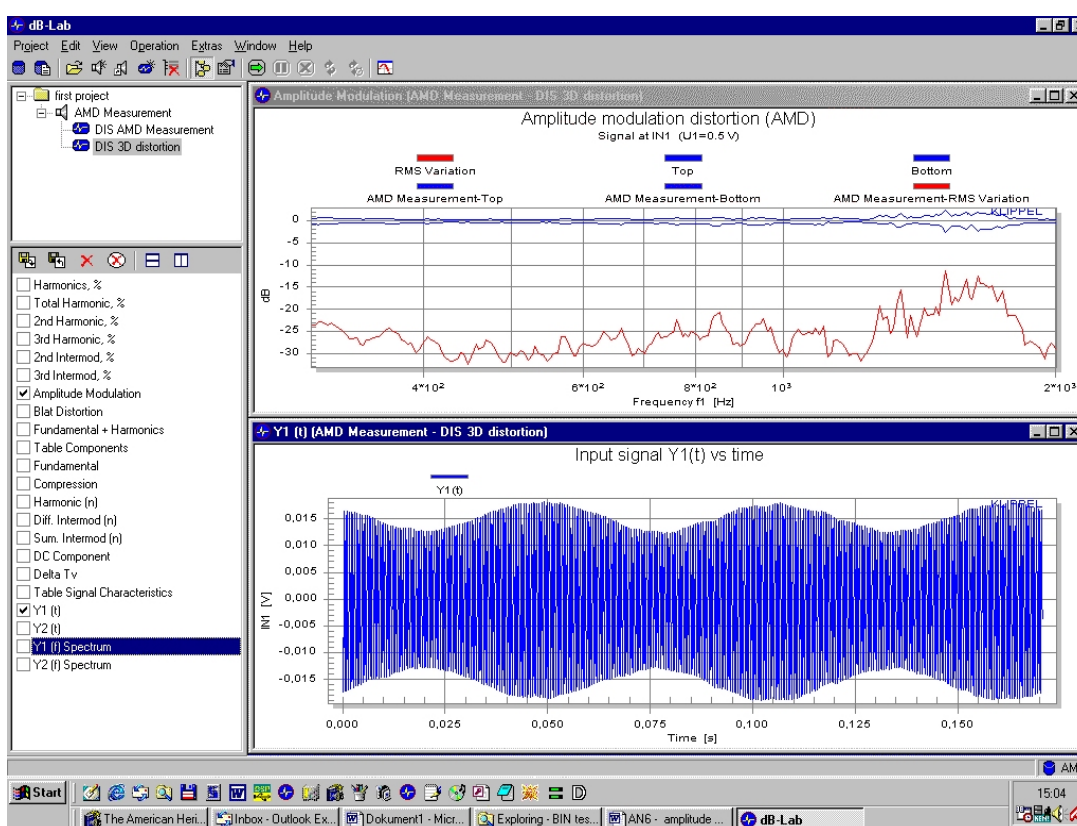


The amplitude modulation of a high frequency tone  $f_1$  (voice tone) and a low frequency tone  $f_2$  (bass tone) is measured by using the 3D Distortion Measurement module (DIS-Pro) of the KLIPPEL R&D SYSTEM. The maximal variation of the envelope of the voice tone  $f_1$  during one period of the bass tone is represented by the top and bottom value referred to the fundamental response measured without bass tone. Both values reveal only the effects of amplitude modulation caused by  $B(x)$ ,  $L_e(x)$  and radiation nonlinearity but are immune against frequency modulation caused by the Doppler Effect. The difference between the amplitude response of the fundamental component  $f_1$  with and without bass tone reveals nonlinear amplitude compression. This measurement is preferred in automotive applications for showing the impact of AM on the generation of intermodulation distortion.



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updated April 4, 2012

<b>Method of Measurement</b>	
<b>Loudspeaker Setup</b>	The loudspeaker shall be operated under free-field or half-space free-field condition. The measurement is to be taken at 1 meter from the speaker (on axis).
<b>1<sup>st</sup> Measurement (Reference)</b>	Measure the frequency response $L_1(f_1) = 20 \log( H_1(f_1) )$ of a 0.5 V rms sine wave, swept from $f_{start} = 200$ Hz (or 4 times resonance frequency $f_s$ ) to 10 kHz at a minimum resolution of 40 points per decade.
<b>2<sup>nd</sup> Measurement (Intermodulation)</b>	The loudspeaker is excited by a two-tone signal. Apply a 2.0 V rms sine wave signal (bass tone) to a frequency $f_2$ of $1/4^{\text{th}}$ of resonance $f_s$ . Apply a 0.5 V rms sine wave (voice tone) at frequency $f_1$ , swept from $f_{start} = 200$ Hz (or 4 times resonance frequency $4f_s$ ) to 10 kHz, applied simultaneously with the bass tone at a minimum resolution of 40 points per decade. Measure the frequency response $L_2(f_1) = 20 \log( H_2(f_1) )$ and the envelope $E[t]$ of the voice tone $f_1$ .
<b>Mean Modulation</b>	Calculate the mean modulation distortion as the difference between the amplitude responses of the voice tone measured with and without the bass tone $f_2$ $M_{mean}(f_1) = L_2(f_1) - L_1(f_1)$ in decibels.
<b>Envelope of <math>f_1</math></b>	The amplitude modulation can be assessed by measuring the variation of the envelope of the high-frequency tone $f_1$ (voice tone) versus one period of the low-frequency tone $f_2$ .  The envelope $E[t]$ of the voice tone $f_1$ is derived from the sound pressure signal $p[t]$ by considering the fundamental of $f_1$ and the summed-tone and difference-tone intermodulation $f_1+(n-1)f_2$ and $f_1-(n-1)f_2$ , respectively, with $2 < n < N$ . If the envelope $E[t]$ is constant over the period $T = 1/f_2$ then the high frequency tone is not amplitude modulated. Frequency modulation caused by the Doppler effect will cause no variation of the envelope $E[t]$ versus $t$ .
<b>Top Envelope</b>	The maximal value of the envelope $E[t]$ over one period $T$ is called top modulation $E_{top} = 20 \log\left(\max_t^{t+T} (E[t])\right)$
<b>Bottom Envelope</b>	The minimal value of the envelope $E[t]$ over one period $T$ is called bottom modulation $E_{bottom} = 20 \log\left(\min_t^{t+T} (E[t])\right)$
<b>Top Modulation</b>	The Top modulation is determined by comparing the maximum of the envelope $E_{top}$ with the amplitude response $L_1(f_1)$ of the reference measurement (without bass tone) $M_{top}(f_1) = E_{top}(f_1) - L_1(f_1)$
<b>Bottom Modulation</b>	The Bottom modulation is determined by comparing the minimum of the envelope $E_{bottom}$ with the amplitude response $L_1(f_1)$ of the reference measurement (without bass tone) $M_{bottom}(f_1) = E_{bottom}(f_1) - L_1(f_1)$
<b>Interpretation</b>	The mean modulation $M_{mean}$ shows the change of sensitivity of the fundamental of the voice tone due to the presence of the bass tone. The force factor $Bl(x)$ and most other nonlinearities will reduce the mean output of the voice tone. Find more information about nonlinear amplitude compression in the reference enclosed.

<b>INTERPRETATION</b>	
<b>The causes for modulation distortion</b>	<p>Exciting with a two-tone signal the loudspeaker produces modulation distortion caused by amplitude and phase (frequency) modulation. Both types of modulation will produce difference intermodulation components at frequencies <math>f_1 - (n-1)f_2</math> and summed-tone intermodulation distortion <math>f_1+(n-1)f_2</math> of nth-order centered around the voice tone <math>f_1</math>. The phase of the intermodulation component depends on the type of modulation. To separate the effect of amplitude modulation from phase modulation the envelope of the high-frequency tone <math>f_1</math> (voice tone) may be investigated. Amplitude modulation only varies the instantaneous amplitude (envelope) of voice tone while not distorting the phase of the voice tone. Contrary, the phase modulation does not change the envelope of the voice tone but varies only the instantaneous phase or frequency.</p> <p>Most of the nonlinearities in drivers such as variation of force factor <math>Bl(x)</math>, inductance <math>L_e(x)</math> versus displacement <math>x</math> cause amplitude modulation. Variation of the radiation conditions causes both amplitude and frequency modulation distortion. The Doppler effect causes phase modulation because the time delay varies with the changed distance between moving diaphragm and fixed listening point.</p>
$M_{top} \approx 0$ $M_{bottom} \approx 0$	<p>If both <math>M_{top} \approx M_{bottom} \approx 0</math> the envelope of <math>f_1</math> is constant and the voice tone is not amplitude modulated by the bass signal <math>f_2</math>. No intermodulation distortion at summed- and difference-frequencies will be generated. This is typical for a linear system but also for nonlinearities (stiffness of the suspension) which do not produce significant intermodulation distortion at higher frequencies.</p>
$M_{top} \approx 0$ $M_{bottom} < 0$	<p>The case <math>M_{top} \approx 0</math> and <math>M_{bottom} &lt; 0</math> is typical for a symmetrical <math>Bl(x)</math> nonlinearity because the sensitivity of the speaker decreases for any movement of the coil away from the rest position. In this case we usually find high values of third-order modulation distortion <math>d_3</math> as defined in IEC 60268.</p>
$M_{top} > 0$ $M_{bottom} < 0$	<p>The case <math>M_{top} &gt; 0</math> and <math>M_{bottom} &lt; 0</math> is typical for an asymmetrical characteristic of <math>Bl(x)</math> or <math>L_e(x)</math> and for radiation distortion. In this case we measure usually high values of second-order modulation distortion <math>d_2</math> as defined in IEC 60268.</p>
$M_{top} < 0$ $M_{bottom} < 0$	<p>The case where both values <math>M_{top}</math> and <math>M_{bottom}</math> are negative is typical for loudspeaker having significant asymmetries in the parameters <math>Bl(x)</math>, <math>K_{ms}(x)</math> or <math>L_e(x)</math> which produce a dc component in the displacement. The may be interpreted as a dynamic offset of the coil position caused by a rectification of the ac excitation signal. Usually the bass tone <math>f_2</math> contributes most to the dc signal. The dynamic dc offset produce complicated interactions between the nonlinearities.</p> <p>For example a perfectly centered coil at the rest position coupled with a very asymmetric suspension may also produce broad band amplitude modulation because the asymmetry in the suspension produces a dc which pushes the coil to the softer side of the <math>K_{ms}(x)</math> characteristic and destroys the optimal coil position. In this case both <math>M_{top}</math> and <math>M_{bottom}</math> may become negative because the coil uses lower values of the B field. The generation of the dc displacement may be monitored on window <b>DC component</b> by using a laser displacement meter and switching to <b>Displacement</b> on the displayed signal on PP Display.</p>

<b>Using the 3D Distortion Measurement (DIS)</b>	
<b>Requirements</b>	<ul style="list-style-type: none"> <li>• Distortion Analyzer + PC</li> <li>• Software module 3D Distortion Measurement (DIS PRO) + dB-Lab</li> <li>• Microphone</li> <li>• laser displacement sensor (optional to measure <math>X_{max}</math>)</li> </ul>

# AN 6

## Measurement of Amplitude Modulation

### Setup



Don't forget  
ear protection!

Connect the microphone to the input IN1 of the Distortion Analyzer. Set the speaker in the approved environment and connect the terminals with SPEAKER 1. Switch the power amplifier between OUT1 and connector AMPLIFIER.

### Preparation

Create a new database within dB-Lab.  
Create a new DRIVER object based on the template object **IM AM Dist. Automotive AN 6**.

### Measurement

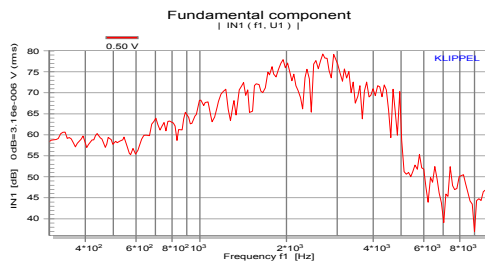
1. Select the created DRIVER and display the operations in the project window. Start the first measurement with the name "**DIS AM 1<sup>st</sup> measurement**"
2. Open the window **Fundamental** of the **DIS AM 1<sup>st</sup> measurement**. Select the displayed curve and copy the curve to the clipboard (mark the curve by clicking on the curve label, press the right mouse button and select **Copy Curve**).
3. Select the **DIS AM 2<sup>nd</sup> measurement** and open the property page **Input**. Import the calibration curve from clipboard (press button **for IN1**) and enable the calibration for Channel 1 (select adjoined checkbox). Check the result window **Calibration Curves** for the correct import of the curve.
4. Start the operation "**DIS AM 2<sup>nd</sup> measurement**".
5. Open the result window **Fundamental + Harmonics** in "**DIS AM 2<sup>nd</sup> measurement**"
6. Print the results or create a report based on the template **IM AM Dist. Automotive AN 6**.

## Customizing Setup Parameters for the DIS Module

<b>Template</b>	Create a new Object, using the object template <b>IM AM Dist. Automotive AN 6</b> in dB-Lab. If this database is not available you may customize a general DIS module according to the following instructions:
<b>DIS AM 1<sup>st</sup> measurement</b>	<ol style="list-style-type: none"> <li>1. Create an object called Driver without any operations assigned (empty object). Assign a measurement <b>DIS AM 1<sup>st</sup> measurement</b> based on the generic <b>DIS 3D distortion module</b>.</li> <li>2. Select the <b>DIS AM 1<sup>st</sup> measurement</b> and open the PP <b>Stimulus</b>. Select mode <b>Intermodulations (f1)</b>. Switch off Voltage Sweep. Set <math>U_{end}</math> to 0.5 V rms. Set <math>U_2/U_1 = -100</math> dB. Set <b>Maximal order of distortion analysis</b> to 10. Switch on the Frequency Sweep with 100 points spaced logarithmically between 200 Hz and 10 kHz. Set frequency of the bass tone to <math>f_2=f_0/4</math>. Set <b>Additional excitation before measurement</b> to 0,1 s.</li> <li>3. Open PP <b>Protection</b>. Disable <b>Monitoring</b> and any protection.</li> <li>4. Open PP <b>Input</b>. Select <b>(Mic) IN1</b> in group <b>(Channel 1) Y1</b> and <b>Off</b> in group <b>(Channel 2) Y2</b>.</li> <li>5. Open PP <b>Display</b>. Select <b>Signal at IN1</b> as <b>State signal</b>.</li> </ol>
<b>DIS AM 2<sup>nd</sup> measurement</b>	<ol style="list-style-type: none"> <li>1. Assign a measurement <b>DIS AM 2<sup>nd</sup> measurement</b> based on the generic <b>DIS 3D distortion</b> module.</li> <li>2. Select the <b>DIS AM 2<sup>nd</sup> measurement</b> and open the PP <b>Stimulus</b>. Select mode <b>Intermodulations (f1)</b>. Switch off Voltage Sweep. Set <math>U_{end}</math> to 0.5 V rms. Set <math>U_2/U_1 = 12</math> dB. Set <b>Maximal order of distortion analysis</b> to 10. Switch on the Frequency Sweep with 100 points spaced logarithmically between 200 Hz and 10 kHz. Set the frequency of the bass tone to <math>f_2=f_0/4</math>. Set <b>Additional excitation before measurement</b> to 0,1 s.</li> <li>3. Open PP <b>Protection</b>. Disable <b>Monitoring</b> and any protection.</li> <li>4. Open PP <b>Input</b>. Select <b>(Mic) IN 1</b> in group <b>(Channel 1) Y1</b> and <b>Off</b> in group <b>(Channel 2) Y2</b>. To measure the displacement generated dynamically select <b>X (Displacement) Y2</b></li> <li>5. Open PP <b>Display</b>. Select <b>Signal at IN1</b> as <b>State signal</b>.</li> </ol>

## Example

### Amplitude Response



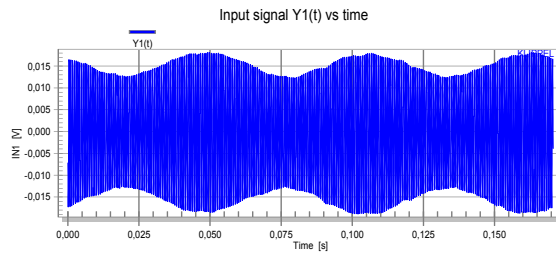
After performing the reference measurement with the voice tone  $f_1$ , the window **Fundamental** shows the amplitude response of the high frequency voice tone  $f_1$  versus frequency.

# AN 6

## Measurement of Amplitude Modulation

### Two-tone Signal

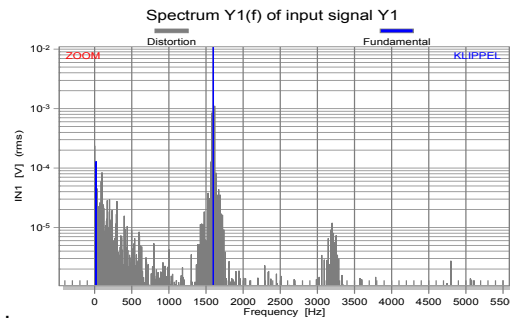
Open the window **Waveform Y1** to see the sound pressure versus measurement time.



This variation of the envelope shows a pure amplitude modulation of the voice tone  $f_1$  according to frequency  $f_2 = 20$  Hz.

### Spectrum

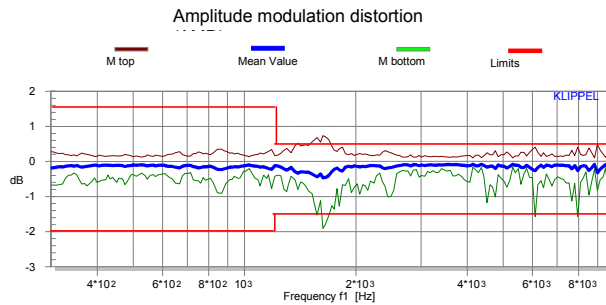
Open the window **Spectrum Y1** to see the spectrum of the reproduced two-tone signal:



The bass tone at  $f_2=20$  Hz causes harmonic distortion at lower frequencies and intermodulation centered around the voice tone at  $f_1 = 1600$  Hz. The distortion above 3 kHz are harmonics of the voice tone  $f_1$ ,

### Amplitude Modulation

The figure below shows the result window **Fundamental + Harmonics** after performing the second measurement.



The top and bottom modulation  $M_{top}$  and  $M_{bottom}$  describe the minimal and maximal variation of the envelope. The mean modulation shows the variation of the amplitude response of the high frequency tone with and without bass tone.

Please note that you may modify or add additional limit curves to the result window by selecting any curve, copying the curve to the clipboard and editing the curve in the clipboard editor provided in dB-Lab and pasting the curve into the diagram. To select curves of interest, right-click the chart, select "Customize...". In the Customization dialog, select the "Subsets" tab, and select the curves to display.

## More Information

<b>Related Application Notes</b>	"3D Harmonic Distortion Measurement", Application Note AN 9 "AM and FM Distortion in Speakers", Application Note AN 10 "Multi-tone Distortion Measurement", Application Note AN 16
<b>Related Specification</b>	"DIS", S4
<b>Software</b>	User Manual for KLIPPEL R&D SYSTEM.
<b>References</b>	M. Ziembra, Position Dependent Amplitude Response in Automotive Loudspeakers, SEA 2000 World Congress Detroit, Michigan, March 6-9, 2000  W. Klippel, "Assessment of Voice Coil Peak Displacement Xmax, paper presented at the 112th Convention of the Audio Engineering Society, 2002 May 10 – 13, Munich, Germany. Updated version on <a href="http://www.klippel.de/know-how/literature/papers.html">http://www.klippel.de/know-how/literature/papers.html</a>

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